

DISPLAY DEVICE

BACKGROUND OF THE INVENTION

Field of the Invention

5 The present invention relates to an observation optical system, and more particularly to an optical system adapted for use in a device called head-up display or spectacle-type display.

Related Background Art

10 Conventionally there have been proposed display devices in which a cathode ray tube (CRT) or a liquid crystal display (LCD) is positioned close to the head of the observer whereby the observer is enabled to observe the image formed by such CRT or LCD, as
15 disclosed for example in U.S. Patent Nos. 4,081,209 and 4,969,724 and Japanese Patent Laid-Open Application Nos. 58-78116, 2-297516 and 3-101709. Japanese Patent Laid-Open Application No. 3-101709 discloses an
20 observation device providing a relatively easily observable real image by re-focusing an original image. However, a considerably large space is unavoidable because an optical lens is employed for re-imaging.

 On the other hand, U.S. Patent Nos. 4,081,209 and 4,969,972 and Japanese Patent Laid-Open
25 Application Nos. 58-78116 and 2-297516 disclose observation devices designed to observe a false image

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which is advantageous for compactizing the device though it is somewhat inferior in the ease of observation.

Though the observation device of the latter type
5 can achieve compactization in comparison with that of the real image type, the extent of such compactization cannot be said sufficient. Among the above-mentioned prior technologies, the one disclosed in the Japanese Patent Laid-Open Application No. 58-78116 is relatively
10 advanced in terms of compactization, but the device still has a large thickness in the direction of the axis of the eye. It is also described that the observed image involves optical distortion, astigmatism and coma. A related technology is also described in
15 U.S. Patent Application Serial No. 08/317,529 filed October 4, 1994.

SUMMARY OF THE INVENTION

In consideration of the foregoing, an object of
20 the present invention is to provide a compact and thin observation optical system.

Another object of the present invention is to provide an observation optical system with reduced aberrations.

25 The above-mentioned objects can be attained, according to an aspect of the present invention, by a display device comprising display means for

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displaying information, and optical means provided with curved faces for guiding the light from said display means to the eye, wherein said optical means has, in succession in the proceeding direction of the eye, a
5 light entrance face for introducing the light, a curved face for totally reflecting the light and a face concave to the eye for reflecting the light toward the eye whereby the light reaches the eye by way of these curved faces and a compact display device can be
10 attained with satisfactorily suppressed aberrations.

Still another object of the present invention is to provide the above-mentioned display device with a visual axis detecting device thereby controlling the display state of said display means.

15 Still other objects of the present invention, and the features thereof, will become fully apparent from the following description of the embodiments.

BRIEF DESCRIPTION OF THE DRAWINGS

20 Figs. 1A and 1B are views showing optical paths in the observation optical system of the present invention;

Figs. 2A and 2B are views showing a cross section and optical paths in the observation optical system of
25 a numerical example 1 of the present invention;

Figs. 3A and 3B are views showing a cross section and optical paths in the observation optical system of

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a numerical example 2 of the present invention;

Figs. 4A and 4B are views showing a cross section and optical paths in the observation optical system of a numerical example 3 of the present invention;

5 Figs. 5A and 5B are views showing a cross section and optical paths in the observation optical system of a numerical example 4 of the present invention;

10 Figs. 6 and 7 are optical cross-sectional views showing the basic principle of the observation optical system of the present invention;

Figs. 8A and 8B are schematic views showing the optical paths of an observation optical system of the present invention;

15 Fig. 9 is a schematic view showing the optical path of a visual axis detecting system employed in the present invention;

Figs. 10 and 11 are schematic views showing states when the display device of the present invention is worn by the observer;

20 Figs. 12A and 12B are partial magnified views of Figs. 8A and 8B;

Fig. 13 is a partial schematic view in the vicinity of a prism member in an embodiment 6 of the present invention;

25 Fig. 14 is a partial schematic view in the vicinity of a prism member in an embodiment 7 of the present invention;

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Fig. 15 is a partial schematic view in the vicinity of a prism member in an embodiment 8 of the present invention;

Fig. 16 is a partial schematic view in the vicinity of a prism member in an embodiment 9 of the present invention;

Figs. 17A and 17B are schematic views showing the optical paths of an observation system and a visual axis detecting system in an embodiment 8 of the present invention;

Figs. 18A and 18B are schematic views showing the optical paths of an observation system and a visual axis detecting system in an embodiment 9 of the present invention;

Figs. 19A and 19B are partial schematic views of an observation optical system and a visual axis detecting optical system, respectively, of the present invention;

Fig. 20 is a flow chart showing the control sequence of the present invention;

Fig. 21 is a schematic view showing selectable display areas in the present invention;

Fig. 22 is a schematic view showing points for display area selection in the present invention;

Figs. 23A and 23B are partial schematic views of an observation optical system and a visual axis detecting optical system, respectively, of the present

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invention; and

Fig. 24 is a flow chart showing the control sequence of the present invention.

5 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

At first there will be explained the basic principle of the display optical system of the present invention, with reference to Figs. 1A, 1B and 6.

Display means 4, for displaying an original image such
10 as a character or a pattern, is composed for example of a known liquid crystal display (LCD) device. There are also provided a first optical member 3a for guiding the light from the display means 4 to the eye of the observer, and a second optical member 3b. The light
15 from the display means 4 at first enters the first optical member 3a, then totally reflected by a totally reflecting face 1, at the eye side, of the first optical member, further reflected by a concave half mirror 2, concave to the eye of the observer,
20 transmitted by the above-mentioned totally reflecting face 1 and guided to the eye.

Figs. 1A and 1B illustrate the optical path, seen respectively from the top and from the side.

As the concave mirror 2 is composed of a half
25 mirror, the observer can observe the image on the display means 4, superimposed with the external scenery. Although the present embodiment provides

a superimposing device, there may also be provided a device for merely observing the image display, in which case the concave mirror is composed of a mirror.

Owing to the above-explained configuration, the present and ensuing embodiments provide extremely thin, compact display devices, with a thickness of the optical system in the order of 10 to 15 mm. Also there is achieved a wide viewing angle of ca. $\pm 16.8^\circ$ in the horizontal direction and ca. $\pm 11.4^\circ$ in the vertical direction.

Such compactization, wide viewing angle and satisfactory optical performance are derived in the present embodiment from fact that a face at the observer side is utilized as a totally reflecting face and a transmitting face, and that the concave mirror 2 is positioned considerably eccentric with respect to the optical axis of the eye. In addition there are significant contributions from facts that the totally reflecting face is constituted by a curved surface, particularly with optical power variable depending on the azimuthal angle as will be shown in the following numerical examples, and that the concave mirror 2 is given an optical power depending on the azimuthal angle.

In particular, the optical power depending on the azimuthal angle, given to the concave mirror 2, allows to sufficiently eliminate the eccentric aberration

Also the totally reflecting face is similarly constituted by a curved surface to correct the aberrations generated by the concave mirror.

For reducing the thickness in the direction of
25 optical axis of the eye, the elements are desirably
so arranged that the optical system 3 stands upright.
More specifically, referring to Fig. 7, there is

For reducing the thickness in the direction of optical axis of the eye, the elements are desirably so arranged that the optical system 3 stands upright. More specifically, referring to Fig. 7, there is

preferably satisfied a condition:

$$|\alpha| \leq 20^\circ$$

wherein α is the angle (tilt angle) of the tangential line to the totally reflecting face 1 at the vertex thereof, to a line perpendicular to the optical axis of the eye. Outside this range, the optical system becomes thicker in the direction of the optical axis, whereby the device becomes bulkier. Also in case of superimposing an image on the scenery, the inclination of the optical member becomes larger to cause a distortion in the observed scenery.

More preferably there is satisfied a condition:

$$-15^\circ \leq \alpha \leq 5^\circ$$

Below the lower limit, the optical system can be made thinner in a direction parallel to the optical axis of the eye, but the distortion becomes severer. Above the upper limit, the optical system becomes thicker in a direction parallel to the optical axis of the eye, and the prisms become undesirably heavy.

In the present embodiment, since the totally reflecting face is concave to the eye, the light entrance face at the outside is constituted by a substantially same curved surface in order to prevent the distortion in the observed scenery.

The concave mirror 2 is made considerably eccentric with respect to the optical axis of the eye, whereby an eccentric aberration is generated.

However this eccentric aberration is satisfactorily corrected by constituting the totally reflecting face with a curved surface and employing, in the concave mirror 2, a surface of which curvature varies depending on the azimuthal angle (toric or anamorphic surface). Preferably an aspherical surface (toric aspherical or anamorphic aspherical surface) to attain an extremely satisfactory optical performances.

With respect to the generatrix direction (y-direction) which is the direction of folding of the light and the meridian direction perpendicular thereto, the faces of the optical system are so designed to have optical powers variable depending on the azimuthal angle, but, in the entire system, the paraxial focal length is preferably substantially constant in any direction. More specifically, there is preferably satisfied a condition:

$$0.9 < |f_y/f_x| < 1.1$$

wherein f_y and f_x are paraxial focal lengths of the entire system respectively along the cross section in the direction of generatrix and that in the direction of meridian.

Also the totally reflecting face (or transmitting face) or the concave mirror is so designed, as explained in the foregoing, as to vary the optical power depending on the azimuthal angle thereby suppressing the eccentric aberration, and, for this

purpose, there is preferably satisfied a condition:

$$|r_x| < |r_y|$$

wherein r_y and r_x are radii of paraxial curvature of said face respectively in the cross section in the generatrix direction and in that in the meridian direction.

In the present embodiment, for achieving compact configuration, the concave mirror 2 is significantly tilted (decentralized) in the direction of generatrix which is the direction of folding of the light, the eccentric aberration is generated larger in the direction of generatrix than in the direction of meridian. Thus the optical power in the cross section in the direction of generatrix is made weaker than that in the cross section in the direction of meridian, namely the radius of paraxial curvature is made longer in the direction of generatrix as indicated in the foregoing condition, thereby suppressing the eccentric aberration in the direction of generatrix.

Preferably these curvatures are so selected as to satisfy:

$$|r_x/r_y| < 0.85$$

Outside this range, the eccentric aberration becomes conspicuously large.

On the other hand, in case the entrance face 5 is so constructed as to have varying optical power depending on the azimuthal angle as in the following

numerical examples 2 to 4, the eccentric aberration can be suppressed by inversely satisfying a condition:

$$|r_x| > |r_y|$$

For further satisfactory correction of
5 aberrations, there are preferably satisfied conditions:

$$-2.0 < 2f_x/r_{x2} < -0.1 \quad \dots (a)$$

$$-2.5 < 2f_x/r_{x3} < -0.5 \quad \dots (b)$$

wherein r_{x2} and r_{x3} are radii of paraxial curvature
respectively of the totally reflecting face (or
10 transmitting face) 1 and the concave mirror 2, in
the cross section in the meridian direction.

Below the lower limit of the condition (a), the
curvature (negative power) of the totally reflecting
face in the meridian direction becomes stronger and the
15 correction of distortion becomes difficult. Also below
the lower limit of the condition (b), the curvature
(positive power) of the concave mirror in the meridian
direction becomes strong and the correction of
astigmatism becomes difficult. On the other hand,
20 above the upper limit of the condition (a), the
curvature of the totally reflecting face in the
meridian direction becomes to have a positive power, so
that the totally reflecting condition becomes difficult
to satisfy. Also above the upper limit of the
25 condition (b), the positive power of the concave mirror
in the meridian direction becomes weaker, so that the
thickness of the optical system in a direction parallel

to the optical axis of the eye becomes undesirably large.

Furthermore, there are preferably satisfied conditions:

$$\begin{aligned} 5 \quad & -1.0 < 2f_y/r_{y2} < 0 & \dots (c) \\ & -2.5 < 2f_y/r_{y3} < -0.2 & \dots (d) \end{aligned}$$

wherein f_y is the focal length of the entire system in the generatrix direction, r_{y2} is the radius of curvature of the totally reflecting face, and r_{y3} is the radius of curvature of the concave mirror.

Below the lower limit of the condition (c), the negative power of the totally reflecting face in the generatrix direction becomes stronger, so that the eccentric distortion becomes difficult to correct.

Below the lower limit of the condition (d), the positive power of the concave mirror in the generatrix direction becomes stronger, thereby generating a large eccentric astigmatism. Also above the upper limit of the condition (c) relating to the totally reflecting condition in the generatrix direction, it becomes difficult to satisfy the totally reflecting condition. Also above the upper limit of the condition (d) relating to the power of the concave mirror in the generatrix direction, this power becomes weaker so that the entire length of the optical system extends in the generatrix direction.

In the foregoing, the structures of the totally

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reflecting face (or transmitting face) 1 and the concave mirror 2 have been explained in relation principally with the curvature, but, in the present embodiment, the concave mirror 2 is subjected to a parallel shift, in the direction of generatrix (y-direction), from the optical axis of the eye toward the original image side (+) as shown in Fig. 7, whereby the eccentric distortion in the generatrix direction can also be suppressed.

10 The eccentric distortion can be suppressed by a parallel shift satisfying:

$$E \geq 2.5 \text{ mm}$$

wherein E is the amount of the parallel shift or the distance from the optical axis of the eye to the vertex of the concave mirror surface in the direction of generatrix (cf. Fig. 7). In the following example 1, this amount E of parallel shift is equal to 5.2 mm, but it may be selected larger as in other examples for satisfactorily correcting the aberrations, and preferably satisfied a condition $E \geq 23 \text{ mm}$.

20 Then, with respect to the entrance face 5, the angle $\theta\beta$ between the entrance face and the original image surface constituting the display means, in the direction of generatrix, is preferably so selected as to satisfy a condition:

$$5^\circ \leq \theta\beta \leq 30^\circ$$

Below the lower limit, the entrance face and the

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original image surface become closer to parallel, so that the original image becomes undesirably thick in the direction parallel to the optical axis of the eye. On the other hand, above the upper limit, the original
5 image becomes perpendicular to the direction parallel to the optical axis of the eye.

The present embodiment assumes, though not illustrated, the use of a rear light source or direct natural light for illuminating the original image.
10 If the original image becomes perpendicular to the above-mentioned optical axis, it becomes difficult to efficiently obtain natural light for direction illumination and the false image obtained by the reflective optical system becomes darker.
15 Consequently the present embodiment utilize the natural light illumination and the back light illumination selectively by detecting the external illumination intensity, thereby utilizing the natural light illumination in the daytime when the natural
20 light is strong and the back light illumination at night.

The display means 4 for forming the original image is composed of a liquid crystal display (LCD) device for compactizing the entire device, and the angle γ
25 between the optical axis at the center of the original image and the principal ray of the light emerging from the original image (central light beam of the diaphragm

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constituted by the eye) (cf. Fig. 7) is preferably so selected as to satisfy:

$$|\gamma| \leq 10^\circ$$

This condition is required in case a liquid crystal display device is employed for providing the original image. The liquid crystal display in general has a narrow viewing angle, the light obliquely entering the display device and emerging therefrom is easily lost. Therefore, a bright false image cannot be obtained unless the light is made to enter the liquid crystal display surface and to emerge therefrom as perpendicularly as possible. The above-mentioned condition allows to observe a sufficiently bright image.

Figs. 2A to 5B are optical cross-sectional views respectively of numerical examples 1, 2, 3, and 4 explained in the following. The configuration shown in Figs. 2A and 2B employs toric aspherical surfaces in the concave mirror and the totally reflecting face. The configuration shown in Figs. 3A and 3B employs anamorphic aspherical surfaces in all of the concave mirror, totally reflecting face and light entrance face. Also the configurations shown in Figs. 4A to 5B employ anamorphic aspherical surfaces in all the optical faces.

In the numerical examples 2 to 4 corresponding to

Figs. 3A to 5B, the entrance face 5 is also provided with a curvature for attaining more satisfactory correction of aberrations.

In the present embodiment, all the optical members are composed of acrylic resin, but glass may naturally be employed instead.

In the following there are shown numerical examples of the present embodiment, wherein TAL indicates a toric aspherical lens face, and AAL indicates an anamorphic aspherical lens face.

The TAL is defined by:

$$z = \frac{y^2/r_i}{1 + \sqrt{1 - (1+k_i)(y/r_i)^2}} + A_i y^4 + B_i y^6 + C_i y^8 + D_i y^{10}$$

wherein i indicates the face number.

Also the AAL is defined by:

$$z = \frac{y^2/r_{iy} + x^2/r_{ix}}{1 + \sqrt{1 - \{(1+k_{iy})(y/r_{iy})^2 + (1+k_{ix})(x/r_{ix})^2\}}} + AR_i \{(1 + AP_i) y^2 + (1 - AP_i) x^2\}^3 + BR_i \{(1 + BP_i) y^2 + (1 - BP_i) x^2\}^4 + CR_i \{(1 + CP_i) y^2 + (1 - CP_i) x^2\}^5 + DR_i \{(1 + DP_i) y^2 + (1 - DP_i) x^2\}^6$$

wherein i indicates the face number.

A_i and B_i are aspherical coefficients.

In the following examples, at least the totally reflecting face is constructed with a face with variable refractive power depending on the azimuthal angle, but it may also be constructed with a rotationally symmetrical spherical or aspherical face.

Example 1

	r_{yi} [mm]	r_{xi} [mm]	y, z		tilt angle in generatrix direction
	radius of curvature in generatrix direction	radius of curvature in meridian direction	coordinates of vertex		
i=1	∞		(0,0)		0
2	-548.019	-74.077	(-0.05, 19.80)	TAL	0
3	-57.595	-40.526	(5.10, 29.14)	TAL	-22
4	-548.019	-74.077	(-0.05, 19.80)	TAL	0
5	∞		(18.58, 28.07)		68.90
6	∞		(21.38, 29.15)		51.17

} in prism

	K_i, K_i	A_i, A_i	B_i, B_i	C_i, C_i	D_i, D_i
(TAL2,4)	613.869	-0.473E-5	0.326E-7	-0.940E-10	0.991E-13

	K_i	A_i	B_i	C_i	D_i
(TAL3)	-1.360	0.345E-5	-0.301E-7	0.944E-10	-0.113E-12

refractive index
(d-line) of prism 1.49171 focal length in
generatrix
direction $f_y = 21.07\text{mm}$

Abbe's number
(d-line) of prism 57.4 focal length in
meridian
direction $f_x = 21.86\text{mm}$

(numerical data)

$$\begin{aligned} \alpha &= -1.8^\circ & E &= 5.2\text{mm} \\ |f_y/f_x| &= 0.96 & \gamma &= 1.36 \\ |r_x/r_y| &= 0.7 & \beta &= 17.7 \\ 2f_x/r_x &= -0.59 \\ 2f_x/r_y &= -1.08 \\ 2f_y/r_x &= -0.08 \\ 2f_y/r_y &= 0.73 \end{aligned}$$

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Example 2

	r_{yi} [mm] radius of curvature in generatrix direction	r_{xi} [mm] radius of curvature in meridian direction	y, z coordinates of vertex	tilt angle in generatrix direction
i=1	∞		(0, 0)	0
2	-2158.074	-32.224	(0.60, 19.83)	-10.55
3	-63.157	-32.870	(34.76, 30.90)	15.81
4	-2158.074	-32.224	(0.60, 19.83)	-10.55
5	72.108	1049.744	(14.82, 29.00)	53.74
6	∞		(17.03, 30.62)	42.91

} in prism

(AAL2, 4)	K_{y1}	K_{x1}	$AR_{1,1}$	$BR_{1,1}$	$CR_{1,1}$	$DR_{1,1}$
	-13763.5	-3.896	-0.170E-4	0.401E-7	-0.154E-9	0.223E-12
			$AP_{1,1}$	$BP_{1,1}$	$CP_{1,1}$	$DP_{1,1}$
			-0.245	0.416E-1	0.870E-1	0.203E-1

(AAL3)	K_{y2}	K_{x2}	AR_2	BR_2	CR_2	DR_2
	1.238	0.279	-0.317E-5	0.248E-8	-0.179E-11	0.608E-15
			AP_2	BP_2	CP_2	DP_2
			0.249	0.327E-2	-0.192E-1	0.181E-1

(AAL5)	K_{y3}	K_{x3}	AR_3	BR_3	CR_3	DR_3
	6.285	-1.33E-6	-0.114E-4	-0.402E-6	0.113E-8	-0.411E-10
			AP_3	BP_3	CP_3	DP_3
			0.273E1	0.155E1	0.160E1	-0.644

refractive index
(d-line) of prism 1.49171 focal length in
generatrix
direction $f_y = 23.20\text{mm}$

Abbe's number
(d-line) of prism 57.4 focal length in
meridian
direction $f_x = 24.09\text{mm}$

(numerical data)

$$\begin{aligned}
 \alpha &= -10.5^\circ & 2f_1/r_{x1} &= -1.5 & 2f_1/r_{x2} &= -0.73 \\
 |f_y/f_1| &= 0.96 & 2f_1/r_{x2} &= -1.47 & E &= 34.1\text{mm} \\
 r_1/r_y &= 0.52 & 2f_1/r_{x3} &= -0.02 & \gamma &= 0.23^\circ \\
 & & & & \beta &= 10.8^\circ
 \end{aligned}$$

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Example 3

	r_{yi} [mm] radius of curvature in generatrix direction	r_{xi} [mm] radius of curvature in meridian direction	y, z coordinates of vertex	tilt angle in generatrix direction
i=1	∞		(0,0)	0
2	-3945.723	-49.792	(3.665, 20.415)	AAL 0.04
3	-67.136	-38.803	(36.403, 32.01)	AAL 14.60
4	-3945.723	-49.792	(3.665, 20.415)	AAL 0.04
5	123.302	843.030	(19.610, 28.357)	AAL 61.72
6	∞		(22.402, 29.859)	52.54

} in prism

(AAL2, 4)	K_{11}	K_{22}	AR_{11}	BR_{11}	CR_{11}	DR_{11}
	7202.73	-7.709	-0.142E-7	0.379E-7	-0.154E-9	0.198E-12
			AP_{11}	BP_{11}	CP_{11}	DP_{11}
			-0.183	0.710E-1	0.514E-1	0.201E-1

(AAL3)	K_{12}	K_{21}	AR_{12}	BR_{12}	CR_{12}	DR_{12}
	1.066	0.193	-0.222E-5	0.321E-8	-0.188E-11	0.461E-15
			AP_{12}	BP_{12}	CP_{12}	DP_{12}
			0.390	0.586E-1	-0.185E-1	-0.222E-1

(AAL5)	K_{13}	K_{31}	AR_{13}	CR_{13}	DR_{13}
	-85.544	-916252	-0.913E-6	-0.204E-9	0.117E-13
			AP_{13}	BP_{13}	CP_{13}
			0.989E1	0.128E1	0.128E2

refractive index
(d-line) of prism 1.49171 focal length in
generatrix direction $f_y = 23.71\text{mm}$

Abbe's number
(d-line) of prism 57.4 focal length in
meridian direction $f_x = 23.70\text{mm}$

(numerical data)

$\alpha = 0.05^\circ$	$2f_x/r_{11} = -0.95$	$2f_y/r_{11} = -0.71$
$ f_y/f_x = 1.0$	$2f_x/r_{22} = -1.22$	$E = 25.6\text{mm}$
$ r_x/r_y = 0.58$	$2f_y/r_{22} = -0.01$	$\gamma = 1.97^\circ$
		$\beta = 15.5^\circ$

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Example 4

	r_{yi} [mm] radius of curvature in generatrix direction	r_{xi} [mm] radius of curvature in meridian direction	y, z coordinates of vertex	tilt angle in generatrix direction	
i=1	∞		(0,0)	0	
2	-3752.581	-50.580	(2.85, 23.13)	AAL	0
3	-66.938	-38.651	(36.37, 34.72)	AAL	14.15
4	-3752.581	-50.580	(2.85, 23.13)	AAL	0
5	306.125	1095.447	(18.59, 31.48)	AAL	69.84
6	∞		(21.46, 32.54)		51.20

} in prism

(AAL2,4)	$K_{x,4}$	$K_{y,4}$	$AR_{x,4}$	$BR_{x,4}$	$CR_{x,4}$	$DR_{x,4}$
	-33820.5	-11.350	-0.144E-4	0.398E-7	-0.153E-9	0.201E-12
			$AP_{x,4}$	$BP_{x,4}$	$CP_{x,4}$	$DP_{x,4}$
			-0.152	0.730E-1	0.494E-1	0.255E-1

(AAL3)	$K_{x,3}$	$K_{y,3}$	$AR_{x,3}$	$BR_{x,3}$	$CR_{x,3}$	$DR_{x,3}$
	1.063	0.127	-0.225E-5	0.316E-8	-0.188E-11	0.474E-15
			$AP_{x,3}$	$BP_{x,3}$	$CP_{x,3}$	$DP_{x,3}$
			0.372	0.568E-1	-0.168E-1	-0.208E-1

(AAL5)	$K_{x,5}$	$K_{y,5}$	$AR_{x,5}$	$BR_{x,5}$	$CR_{x,5}$	$DR_{x,5}$
	745.334	-651374	-0.656E-6	0.124E-6	0.474E-12	-0.972E-11
			$AP_{x,5}$	$BP_{x,5}$	$CP_{x,5}$	$DP_{x,5}$
			0.837E1	-0.273	0.563E1	-0.538

refractive index
(d-line) of prism 1.49171 focal length in
generatrix
direction $f_y = 23.09\text{mm}$

Abbe's number
(d-line) of prism 57.4 focal length in
meridian
direction $f_x = 23.09\text{mm}$

(numerical data)

$\alpha = 0^\circ$	$2f_1/r_{x2} = -0.91$	$2f_1/r_{x2} = -0.69$
$ f_1/f_2 = 1.0$	$2f_1/r_{x2} = -1.19$	$E = 33.5\text{mm}$
$ r_1/r_2 = 0.58$	$2f_1/r_{x2} = -0.01$	$\gamma = 1.52^\circ$
		$\beta = 18.6^\circ$

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5 an extremely small thickness of 10 to 15 mm in the
direction parallel to the optical axis of the eye.
It also provides satisfactorily bright optical
performance. Furthermore, by constituting the concave
mirror with a half-transmitting face, it is rendered
0 possible to superimpose a bright false image of the
original image with the scenery without distortion.

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of the systems shown in Figs. 8A and 8B, and Figs. 10 and 11 are schematic views showing the mode of use when the device of the present invention is mounted on the head of the observer.

5 In these drawings, there are shown an observer 101, display means 4 composed for example of a liquid crystal display device and serving to display image information in the visible wavelength region, based on signals from image information supply means such as a
10 CD-ROM 105 or a video camera 106, and an optical member 10 consisting of a transparent parallel-faced flat plate and incorporating therein a dichroic mirror 7 serving as a beam splitter for transmitting the visible light and reflecting the infrared light. The dichroic
15 mirror 7 may however be replaced by a simple half mirror.

 A prism member 3 is provided with a front face 1 consisting of a toric aspherical surface and effecting total reflection in a part; a rear face 6 consisting
20 of a transparent or opaque, flat or curved surface; a concave face 2 consisting of a semi-transmitting or mirror-reflecting toric aspherical surface provided in the prism member 3; and an entrance face 5. An optical axis (central axis) 104 coincides with the optical axis
25 of the eye 103. The elements in the optical path from the display means 4 to the eye 103 constitute an observation system, for observing a false image of the

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image information displayed on the display means 4.
Light source means 102 project infrared light
(wavelength of about 880 nm) to the eye 103 so as to
form Pulkinye's images, in order to detect the visual
5 line of the eye 103 of the observer 101.

When the infrared light from the light source
means 102 is projected onto the eye 103 of the observer
101 as shown in Fig. 8B, an imaging optical system
(imaging lens) 8 forms a corneal reflected image,
10 formed by the light reflected from the cornea of the
eye 103, and images of pupil etc. on an image sensor
9 such as a CCD, through the prism member 3 and the
dichroic mirror 7 of the optical member 10.

The imaging lens 8 is provided independently from
15 the observation system for observing the false image
of the image information of the display means 4.

The elements in the optical path from the light source
means 102 to the image sensor 9 by way of the eye 103
constitute a visual line detecting system for detecting
20 the visual line of the eye 103 of the observer 101.

In the present embodiment, the elements of the
observation system and the visual line detecting
system are designed as explained in the foregoing,
thereby facilitating the compactization of the entire
25 system incorporating these two systems.

In the following there will be explained, with
reference to Figs. 8A and 8B, the observation system

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for observing the false image of the image information
displayed on the display means 4. In the present
embodiment, a visible light beam based on the image
information displayed on the display means 4 is
5 transmitted by the dichroic mirror face 7 of the
optical member 10 and is introduced into the prism
member 3 through the entrance face 5 thereof. It is
then totally reflected by the front face 1 of the prism
member 3, then reflected and condensed by the concave
10 face 2, further transmitted by the front face 1 and
guided to the eye 103 of the observer 101. In such
configuration, the curvatures of the front face 1 and
the concave face 2 are so suitably selected that a
false image of the image information displayed on the
15 display means 4 is formed in front of the observer 101,
without a primary image plane for intermediate image
formation.

As explained above, in the present embodiment, the
observation system is constructed as false image type,
20 whereby the observer 101 observes the false image of
the image information. It is also possible, in the
present embodiment, to constitute the concave face 2
with a semi-transmitting surface and the rear face 6
with a transmitting surface, and suitably selecting
25 the curvature of the rear face 6, thereby spatially
superimposing the external image information and the
false image of the image information of the display

FIG. 10

means 4 for observation in a same viewing field with same visibility.

In the observation system of the present embodiment, in displaying the image information on the display means from the image information supply means such as a CD-ROM 105 or a video camera 106 held by the observer 101 as shown in Figs. 10 and 11, the visual line information of the eye of the observer, obtained by the visual line detecting system, is utilized for various controls, such as auto focusing (focusing of the video camera), electronic zooming (electrical enlargement of the information in the direction of the visual line), zooming (calculation of the focal length f of the video camera for obtaining an image frame size extracted by the visual line and matching to said focal length), and menu selection (light metering, flash panorama size etc.) selected by the visual line.

In the following there will be explained, with reference to Fig. 9, the visual line detecting system for detecting the visual line of the eye 103 of the observer 101. The eye 103 of the observer 101 is illuminated with the infrared light from the light source means 102, and the infrared light reflected by the cornea of the eye 103 is transmitted by the front face 1 of the prism member 3, then reflected by the concave face 2, further totally reflected by the front

face 1, transmitted by the entrance face 5 and guided into the optical member 10. It is then reflected by the dichroic mirror face 7 thereof, totally reflected by a face 10a thereof and is guided to the image sensor 9 through the imaging lens 8.

The imaging lens 8 forms the corneal reflected image and the images of the pupil etc. of the eye 103 on the image sensor 9, and the visual line of the eye 103 is detected from the signal of said image sensor 9.

In the present embodiment, the visual line of the eye is detected by a method disclosed for example in the Japanese Patent laid-Open Application Nos. 1-274736 and 3-11492 of the present applicant.

Figs. 12A and 12B are schematic cross-sectional views of the prism member 3 employed in the present embodiment. It is employed in this case as an observation system, but, in case it is employed as the visual line detecting system, the optical functions remain some except that the optical path is reversed.

A light beam 4a, perpendicularly emitted from the display face of the display means 4 is transmitted by the entrance face 5 of the prism member 3 and enters the toric aspherical front face 1 with an incident angle at least equal to 43° , thereby being totally reflected by said front 1. The light beam 4a is then introduced into the toric aspherical concave face 2 with an incident angle not exceeding 43° , thereby being

reflected by the concave face and is emitted from the front face 1.

The front face 1 is curved, and effects total reflection in a part and transmission in another part.

5 It is therefore equivalent to two curved surfaces, and, in combination with the concave face 2, there is constituted a reflective optical system having three curved surfaces. In this manner the focal length of the entire optical system is shortened (20 to 25 mm in
10 the following numerical examples), whereby the entire optical system can be compactized.

In the present embodiment, a toric surface, a toric aspherical surface or an anamorphic aspherical surface with variable refractive power, i.e. variable
15 curvature, depending on the azimuthal angle is employed in the front face 1, the concave face 2 and the entrance face 5 in the observation system and the visual line detecting system 5, whereby satisfactory correction is attained for the eccentric aberration
20 generated when the angle between the incident light and the emerging light of the concave mirror 2 is made large in order to reduce the size of the entire optical system.

The curvatures of the front face 1 and the rear
25 face 6 are so selected as to constitute a meniscus lens having a small refractive power for the light passing through these faces, whereby the external image

information such as the external scenery can be satisfactorily observed through the rear face 6.

Also in the cross section in the meridian direction, the front face 1 is given a negative refractive power, in order to correct the aberrations generated by the positive refractive power of the concave face 2. The meridian direction means a plane perpendicular to the plane containing the optical path from the center of the image on the display means to the designed center of the eye (i.e. direction perpendicular to the plane of Figs. 12A and 12B).

Also in the present embodiment, the front face 1 may be given a negative refractive power in the cross section in the generatrix direction, for attaining an effect similar to that of the negative refractive power in the cross section in the meridian direction. The cross section in the generatrix direction means a plane containing the optical path from the center of the image of the display means to the designed center of the eye (i.e. plane of Figs. 12A and 12B).

There is satisfied a condition:

$$|\alpha| \leq 20^\circ \quad \dots (1)$$

wherein α is the tilt angle, as shown in Fig. 12B, between a tangential line L at the vertex of the front face 1 in the cross section in the generatrix direction and a line m perpendicular to the optical axis 104 of the eye and passing the vertex of the front face 1.

As indicated by the condition (1), the angle α is selected smaller than 20° , thereby reducing the distortion in observation of the false image of the image information of the display means 4 and the external image information such as external scenery in spatially superimposed state, and reducing the thickness of the prism in the axial direction.

In the following there will be explained other features of the observation system and the visual line detecting system including the elements (entrance face 5, front face 1 and concave face 2) provided in the optical path from the display means 4 to the eye 103.

(2-1) In the present embodiment, the imaging magnification β of the imaging lens 8 from the eye 103 to the image sensor 9 is defined by:

$$0.02 < |\beta| < 0.18 \quad \dots (2)$$

Above the upper limit of the condition (2), the magnification of the eye image becomes too large, so that the effective diameter of the image sensor becomes undesirably large. Also below the lower limit of the condition (2), the focal length of the visual line detecting system has to be made shorter, whereby various aberrations are generated and a satisfactory eye image cannot be obtained.

(2-2) Also there is satisfied a condition:

$$0.9 < |f_y/f_x| < 1.1 \quad \dots (3)$$

wherein f_y , f_x are focal lengths of the entire system

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respectively in the generatrix cross section and the meridian cross section, thereby maintaining a substantially constant focal length for the entire system in any azimuthal angle and dispensing with the correction for the aspect ratio, in the generatrix direction and the meridian direction, of the image information displayed on the display means.

(2-3) Also there is satisfied a condition:

$$|R_x| < |R_y| \quad \dots (4)$$

wherein R_y , R_x are radii of paraxial curvature of the concave face 2 respectively in the generatrix cross section and the meridian cross section.

For compactizing the observation system, the optical axis of the concave face has to be significantly tilted clockwise, in the generatrix cross section, from the optical axis of the eye, but such configuration generates a large eccentric aberration. On the other hand, in the meridian cross section, such eccentric aberration is not generated much because there is little room for such eccentricity. In the present embodiment, therefore, the radius R_y of curvature in the generatrix cross section is selected larger than that R_x in the meridian cross section as indicated by the condition (4), or the refractive power in the generatrix direction is selected weaker than that in the meridian direction, thereby suppressing the eccentric aberration in the generatrix

In the present embodiment, for the purpose of correction of the eccentric aberration, the condition (4) is preferably set as follows:

(2-4) When the entrance face 5 of the prism

$$|R_{y5}| < |R_{x5}| \quad \dots (6)$$

(2-5) Satisfactory optical performance is realized in the meridian cross section by giving a negative refractive power to the totally reflecting area of the front face 1, a positive refractive power to the concave face 2 and a negative refractive power to the transmitting area of the front face 1. In case the entrance face 5 has a refractive power, it is

preferably selected as positive in the generatrix cross section, in order to cover the deficiency in the positive refractive power in the generatrix cross section in the entire system.

5 (2-6) Satisfactory optical performance is realized in the generatrix cross section by giving a negative refractive power in the totally reflecting area of the front face 1, and a positive refractive power to the concave face 2. In case the entrance face 10 5 has a refractive power, it is selected as positive in the meridian cross section, thereby reducing the aberrations in the meridian cross section.

(2-7) In the meridian cross section, there are satisfied condition:

15
$$0.1 < |2f_x/R_{x1}| < 2.0 \quad \dots (7)$$

$$0.5 < |2f_x/R_{x2}| < 2.5 \quad \dots (8)$$

wherein R_{x1} , R_{x2} are radii of curvature respectively of the totally reflecting area of the front face 1 and of the concave face 2, and f_x is the focal length of the entire system. The upper limits of the conditions (7), 20 (8) correspond to stronger refractive forces of said curvatures, while the lower limits correspond to the weaker refractive forces. Above the upper limit of the condition (7), the distortion aberration becomes 25 difficult to correct, and, below the lower limit, the totally reflecting condition becomes difficult to satisfy. Also above the upper limit of the condition

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(8), the astigmatism becomes difficult to correct, and, below the lower limit, the entire optical system becomes larger, particularly with a larger thickness in the direction parallel to the optical axis.

5 (2-8) In the generatrix cross section, there are satisfied condition:

$$0 < |2f_y/R_{y1}| < 1.0 \quad \dots (9)$$

$$0.2 < |2f_y/R_{y2}| < 2.5 \quad \dots (10)$$

10 wherein R_{y1} , R_{y2} are radii curvature respectively of the totally reflecting area of the front face 1 and the concave face 2, and f_y is the focal length of the entire system. The upper limits of the conditions (9) and (10) correspond to stronger refractive powers of said curvatures, while the lower limits correspond to weaker refractive powers. Above the upper limit of the
15 condition (9), the eccentric distortion aberration becomes difficult to correct, while, below the lower limit, it becomes difficult to satisfy the totally reflecting condition. Also above the upper limit of
20 the condition (10), eccentric astigmatism is generated significantly, and, below the lower limit, the length of the entire lens increases and the entire optical system becomes undesirably bulky.

25 (2-9) The concave face 2 is shifted in parallel manner, in the generatrix cross section (Y-direction), from the optical axis 104 of the eye toward the display means 4, thereby suppressing the eccentric distortion

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12B) is so selected as to satisfy:

thereby satisfactorily correcting the eccentric distortion.

$$10 \quad -15^\circ \leq \alpha \leq 5^\circ \quad \dots (12)$$

Figs. 13 to 16 are schematic views showing modifications in a part of the visual line detecting system in the vicinity of the prism member 3.

In an embodiment shown in Fig. 14, the dichroic

face 7 is provided in inclined manner inside the prism member 3, with corresponding positioning of the imaging lens 8 and the image sensor 9. This embodiment is featured by a reduced number of components, leading to further compactization of the entire optical system.

In an embodiment shown in Fig. 15, the optical member 10 is positioned farther than the prism member 3 from the eye 103. Also the concave face 2 is provided with a dichroic film reflecting the visible light and transmitting the infrared light. The optical member 10 is provided with an inclined reflecting face 11, having a semi-transmitting, totally reflecting or dichroic film, and the imaging lens 8 and the image sensor 9 are positioned accordingly. The state of mounting of the device of the present embodiment, on the head of the observer, is schematically illustrated in Figs. 17A and 17B.

In an embodiment shown in Fig. 16, the optical member 10 consisting of a parallel-faced flat plate is replaced by a dichroic mirror 7, transmitting the visible light and reflecting the infrared light, provided on the entrance face 5 of the prism member 3, and the imaging lens 8 and the image sensor 9 are positioned accordingly. The state of mounting of the device of the present embodiment, on the head of the observer, is schematically illustrated in Figs. 18A and 18B.

Display devices utilizing the visual line detecting systems of the above-explained embodiments can be directly applied to so-called head-up display device.

5 In the following there are shown numerical examples of the present embodiment, wherein elements of the system are represented as follows, with reference to Figs. 8A, 8B and 9:

10 (1) eye 103 being selected as the original point (0, 0) of the coordinate system;

 (2) in the visual line detecting system, in tracing the light from the eye 103;

 i = 1 eye
 i = 2 front face 1 (transmitting face)
15 i = 3 concave face 2
 i = 4 front face (totally reflecting face)
 i = 5 entrance face 5
 i = 6 entrance face of optical member 10
 i = 7 dichroic face
20 i = 8
 i = 9 exit face of optical member 10
 i = 10 entrance face of imaging lens
 i = 11 exit face of imaging lens
 i = 12 image sensor
25 in the observation system;
 i = 8 entrance face of image information
 i = 9 display face of image information

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(3) TAL indicates a toric aspherical surface;
and AAL indicates an anamorphic aspherical surface.

The TAL is defined, in the generatrix (Y - Z)
cross section, by the following aspherical equation:

$$Z = \frac{y^2/ryi}{1 + \sqrt{1 - (1+ki)(y/ryi)^2}} + Aiy^4 + Biy^6 + Ciy^8 + Diy^{10}$$

wherein i indicates the face number, and is spherical
in the meridian (X - Z) cross section.

Also the AAL is defined by:

$$Z = \frac{y^2/ryi + x^2/rix}{1 + \sqrt{1 - \{(1+kyi)(y/ryi)^2 + (1+kxi)(x/rix)^2\}}} \\ + ARi\{(1+APi)y^2 + (1-APi)x^2\}^2 + BRi\{(1+BPi)y^2 + (1-BPi)x^2\}^3 \\ + CRi\{(1+CPi)y^2 + (1-CPi)x^2\}^4 + DRi\{(1+DPi)y^2 + (1-DPi)x^2\}^5$$

wherein i indicates the face number.

Also in the present invention, AL indicates a
rotationally symmetrical aspherical surface, which is
defined by:

$$Z = \frac{y^2/ryi}{1 + \sqrt{1 - (1+ki)(y/ryi)^2}} + Aiy^4 + Biy^6 + Ciy^8 + Diy^{10}$$

wherein i indicates the face number. The surface
vertex coordinate (Y, Z) is an absolute coordinate when
the vertex of the eye surface is taken as (0, 0). The
tilt angle in the generatrix cross section indicates

the tilt angle of the optical axis of each face, with respect to the optical axis of the eye, said angle being taken positive anticlockwise. A reflecting face (including totally reflecting face) is indicated by a
5 suffix M. nd and vd respectively indicate the refractive index and the Abbe's number for d-line.

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[Numerical Example 5]

(Visual line detecting system)

r_{yi} Radius of curvature in generatrix cross section	r_{xi} Radius of curvature in meridian cross section	Vertex coordinate Y, Z	Tilt angle in generatrix cross section		
i= 1 ∞		(0, 0)	0 °	eye	
i= 2 -514.575	-52.805	(0, 21.15)	0	TAL	nd=1.49171 ν d=57.4
i= 3 -63.546	-42.575	(26.30, 35.96)	-3.33	TAL-M	
i= 4 -514.575	-52.805	(0, 21.15)	0	TAL-M	
i= 5 ∞		(20.72, 28.06)	65.37		nd=1.51633 ν d=64.1
i= 6 ∞		(21.18, 28.27)	65.37		
i= 7 ∞		(23.41, 28.20)	30.37	M	
i= 8 ∞		(21.18, 28.27)	65.37	M	
i= 9 ∞		(24.93, 20.09)	-54.64		nd=1.49171 ν d=57.4
i=10 -1.889		(26.90, 21.14)	-54.64	AL	
i=11 1.426		(29.35, 19.41)	-54.64	AL	
i=12 ∞		(30.51, 18.95)	-51.60	image sensor	

(Observation system)

i= 8 ∞	(23.91, 29.52)	65.37	nd=1.51633 ν d=64.1	
i= 9 ∞	(24.98, 30.01)	59.37		image information

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(TAL, AL data)

TAL2, 4:K=460.670, A=-0.227E-5, B=0.179E-7, C=-0.453E-10, D=0.429E-13

TAL3 : K=1.105, A=-0.709E-6, B=-0.273E-8, C=-0.191E-11, D=0.631E-15

AL10 : K=-3.858, A=0.851E-2, B=-0.101, C=0.149, D=-0.755E-1

AL11 : K=-0.113, A=0.195, B=-0.590, C=0.471, D=-0.138

(1) $\alpha = 0$ (5) $|R_{x1}/R_{y1}| = 0.10$ (8) $2f_x/R_{x2} = -1.09$ (11) $E = 26.3$

$$(2) \quad |\beta| = 0.10 \quad |R_{x2}/R_{y2}| = 0.67 \quad (9) \quad 2f_{y2}/R_{y1} = -0.04$$

(3) $|f_y/f_x| = 1.00$ (7) $2f_x/R_{x1} = -0.88$ (10) $2f_y/R_{y2} = -0.36$

[Numerical Example 7]

(Visual line detecting system)

r_{yi} Radius of curvature in generatrix cross section	r_{xi} Radius of curvature in meridian cross section	Vertex coordinate Y, Z	Tilt angle in generatrix cross section		
i= 1 ∞		(0, 0)	0 °	eye	
i= 2 -2158.074	-32.224	(0.60, 19.85)	-10.55	AAL	nd=1.49171 $\nu d=57.4$
i= 3 -63.157	-32.870	(34.76, 30.92)	15.81	AAL-M	
i= 4 -2158.074	-32.224	(0.60, 19.85)	-10.55	AAL-M	
i= 5 72.108	1049.744	(14.82, 29.02)	53.74	AAL	
i= 6 ∞		(14.98, 29.14)	53.74		nd=1.51633 $\nu d=64.1$
i= 7 ∞		(17.19, 29.51)	18.74	M	
i= 8 ∞		(14.98, 29.14)	53.74	M	
i= 9 ∞		(20.31, 21.88)	-66.27		
i=10 -1.889		(22.03, 23.31)	-66.27	AL	nd=1.49171 $\nu d=57.4$
i=11 1.426		(24.77, 22.10)	-66.27	AL	
i=12 ∞		(25.96, 21.91)	-63.23	image sensor	

(Observation system)

i= 8 ∞	(17.40, 30.91)	53.74	nd=1.51633 $\nu d=64.1$	
i= 9 ∞	(18.21, 31.50)	44.74		image information

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(AAL, AL data)

AAL2, 4:

Ky=-13763.5, AR=-0.170E-4, BR=0.406E-7, CR=-0.154E-9, DR=0.223E-12

Kx=-3.896, AP=-0.245, BP=0.416E-1, CP=0.870E-1, DP=-0.203E-1

AAL3:

Ky=1.238, AR=-0.317E-5, BR=0.248E-8, CR=-0.179E-11, DR=0.608E-15

Kx=0.279, AP=-0.249, BP=0.327E-2, CP=-0.192E-1, DP=0.181E-1

AAL5:

Ky=6.825, AR=-0.114E-4, BR=-0.402E-6, CR=0.113E-8, DR=-0.411E-10

Kx=-1.33E+6, AP=0.273E+1, BP=0.155E+1, CP=0.160E+1, DP=-0.644

AL10 : K=-3.858, A=0.851E-2, B=-0.101, C=0.149, D=-0.755E-1

AL11 : K=-0.113, A=0.195, B=-0.590, C=0.471, D=-0.138

(1) $\alpha = -10.5$ (5) $|R_{x1}/R_{y1}| = 0.01$ (8) $2f_x/R_{x2} = -1.47$ (11) $E = 34.8$

(2) $|\beta| = 0.12$ $|R_{x2}/R_{y2}| = 0.52$ (9) $2f_y/R_{y1} = -0.02$

(3) $|f_y/f_x| = 0.96$ (7) $2f_x/R_{x1} = -1.5$ (10) $2f_y/R_{y2} = -0.73$

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[Numerical Example 8]

(Visual line detecting system)

r_{yi}	r_{xi}
Radius of	Radius of
curvature	curvature
in generatrix	in meridian
cross section	cross section

Vertex	Tilt angle in
coordinate Y, Z	generatrix
	cross section

i= 1	∞	(0, 0)	0 °	eye		
i= 2	-9423.260	-47.769	(0, 20.38)	1.50	AAL	
i= 3	-65.701	-36.469	(33.13, 29.99)	14.29	AAL-M	nd=1.49171 ν d=57.4
i= 4	-9433.260	-47.769	(0, 20.38)	1.50	AAL-M	
i= 5	7188.930	-49.971	(16.33, 26.54)	62.55	AAL	
i= 6	∞	(19.89, 27.27)	21.55	M		
i= 7	-1.889	(21.28, 20.34)	-11.45	AL	nd=1.49171 ν d=57.4	
i= 8	1.426	(21.88, 17.39)	-11.45	AL		
i= 9	∞		-8.45	image sensor		

(Observation system)

i= 7	∞	(21.11, 29.03)	55.43	image information
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AAL2, 4:

Kx=-13.802, AP=-0.317, BP=-0.602E-1, CP=0.272E-1, DP=-0.211E-1

Kx=0.172, AP=0.472, BP=0.553E-1, CP=-0.265E-1, DP=0.751E-2

$$K_x = -70.169, \quad AP = 41.763, \quad BP = -0.395, \quad CP = 0.183E+2, \quad DP = -0.988$$

AL8 : $K=-0.113$, $A=0.195$, $B=-0.590$, $C=0.471$, $D=-0.138$

$$(2) \quad |\beta| = 0.10 \quad |R_{x2}/R_{y2}| = 0.56 \quad (9) \quad 2f_y/R_{y1} = -0.46$$

(3) $|f_y/f_x| = 1.00$ (7) $2f_x/Rx1 = -0.93$ (10) $2f_y/Ry2 = -0.61$

[Numerical Example 9]

(Visual line detecting system)

r_{yi}	r_{xi}
Radius of	Radius of
curvature	curvature
in generatrix	in meridian
cross section	cross section

Vertex	Tilt angle in
coordinate Y, Z	generatrix
	cross section

i= 1	∞	(0, 0)	0 °	eye		
i= 2	-9538.246	-47.590	(0, 21.30)	7.28	AAL	
i= 3	-65.6	-36.035	(32.96, 31.40)	14.67	AAL-M	nd=1.49171 ν d=57.4
i= 4	-9538.246	-47.590	(0, 21.30)	0.28	AAL-M	
i= 5	225.188	727.642	(16.47, 28.45)	65.28	AAL	
i= 6	∞	(16.92, 28.60)	67.28			nd=1.51633 ν d=64.1
i= 7	∞	(19.15, 28.51)	35.28	M		
i= 8	∞	(16.92, 28.66)	67.28	M		
i= 9	∞	(19.69, 29.82)	67.28	M		
i=10	∞	(23.55, 20.60)	-167.72			
i=11	1.889	(21.38, 20.05)	-167.72	AL		nd=1.49171 ν d=57.4
i=12	-1.426	(20.74, 17.12)	-167.72	AL		
i=13	∞	(20.19, 16.01)	-164.69		image sensor	
(Observation system)						nd=1.51633 ν d=64.1
i= 8	∞	(19.69, 29.82)	67.28			
i= 9	∞	(22.02, 29.17)	54.10		image information	

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(AAL, AL data)

AAL2, 4:

Ky=-387540, AR=-0.183E-4, BR=0.378E-7, CR=-0.117E-9, DR=0.158E-12

Kx=-20.897, AP=-0.300, BP=-0.548E-1, CP=0.326E-1, DP=-0.228E-1

AAL3:

Ky=1.213, AR=-0.224E-5, BR=0.305E-8, CR=-0.190E-11, DR=0.500E-15

Kx=0.165, AP=-0.464, BP=0.630E-1, CP=-0.251E-1, DP=0.380E-2

AAL5:

Ky=559.028, AR=-0.675E-5, BR=0.182E-6, CR=0.212E-12, DR=-0.189E-10

Kx=-99429.4, AP=0.486E+1, BP=-0.125E+1, CP=0.111E+2, DP=-0.789

AL11 : K=-3.858, A=0.851E-2, B=-0.101, C=0.149, D=-0.755E-1

AL12 : K=-0.113, A=0.195, B=-0.590, C=0.471, D=-0.138

(1) $\alpha = 0.28$ (5) $|R_{x1}/R_{y1}| = 0.005$ (8) $2f_x/R_{x2} = -1.26$ (11) $E = 33.0$

(2) $|\beta| = 0.11$ $|R_{x2}/R_{y2}| = 0.55$ (9) $2f_y/R_{y1} = -0.005$

(3) $|f_y/f_x| = 1.00$ (7) $2f_x/R_{x1} = -0.95$ (10) $2f_y/R_{y2} = -0.69$

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According to the present invention, as explained in the foregoing, there is provided a display device, such as a head-mount display, enabling compactization and provided with a visual line detecting system
5 capable of controlling, based on the visual line information, the observation state of the image information displayed by the display means in the observation system, by suitably designing said observation system for observing the image information
10 displayed by the display means and the visual line detecting system provided, in a part of the observation system, for detecting the visual line of the observer.

In the following there will be explained the control of the display device utilizing the above-
15 explained visual line detecting function.

Figs. 19A and 19B show the optical paths respectively of the observation system and the visual line detecting system in the optical system of the present invention.

20 Display means 4 displays, on a display face thereof, an image such as a character or a pattern, with visible light, a flat prism 10 is composed of two adhered prisms, of which junction plane is provided with a dichroic mirror transmitting the visible light
25 and reflecting the infrared light for visual line detection. The prism 10 has a lateral wall 13.

A first optical member 3A is provided with a flat

face 5, a curved or aspherical face 1, and a half-transmitting or totally reflecting, spherical or aspherical face 2a of a positive refractive power.

In the present embodiment, the face 2a is composed of
5 a half mirror. A second optical member 3B is provided with a transparent or opaque, flat or curved face 6, and a concave face 2b, consisting of a half-transmitting or totally reflecting, spherical or aspherical surface same in shape as the face 2a.

10 The face 2a of the first optical member 3A and the face 2b of the second optical member 3B are adhered to constitute a single prism block 3. The adhered face 2 constitutes a half mirror.

There are also provided an imaging lens 8 for
15 visual line detection, an image sensor 9 consisting of a CCD, and a light source 12 for detecting the visual line of the eye E of the observer, by illuminating the frontal part of said eye E with invisible (infrared) light.

20 A visual line detecting circuit 14 detects the visual line information of the eye E. Discrimination means 15 discriminates whether the visual line of the observer is fixed for a predetermined time in a substantially same direction. Control means 16
25 receives image signals from an image information source S and displays an image on the display face of the display means 4 under controlled display state based on

the visual line information from the discrimination means 15.

The prism 10 and the first optical member 3A constitute a part of the image observation optical system, and the image observation optical system and the second optical member 3B constitute a part of the observation optical system.

In the following there will be explained, with reference to Fig. 19A, the function of the observation optical system of the present embodiment. The control means 16 displays the image on the display face of the display means 4, based on the signals from the image information source S. The light beam (visible light beam) from the image displayed on the display means 4 is transmitted by the dichroic mirror 7 of the prism 10, then introduced into the prism block 3 through the face 5, totally reflected by the face 1, then reflected and condensed by the half mirror surface 2, and emerges from the face 1 to enter the pupil 0 of the observer. Thus a false image Y of the image displayed on the display means 4 is formed in front of the observer, and can be observed by the observer.

On the other hand, the light beam from the external scenery G is introduced into the face 6 of the prism block 3, then transmitted by the half mirror 2 and emerges from the face 1 to reach the pupil of the observer, who can thus observe the external scenery.

Thus the observer observes, within a same viewing field, the false image Y of the image displayed on the display means 4 and the external scenery in superposition.

5 In the following there will be explained the function of the visual line detecting optical system of the present embodiment. Referring to Fig. 17B, the light reflected and scattered by the frontal part of the eye E of the observer, illuminated by the infrared
10 light from the light source 12, is introduced into the face 1 of the prism block 3, then reflected by the half mirror 2 toward the face 1, then totally reflected by the face 1 and emerges from the face 5 to enter the prism 10. It is then reflected by the dichroic mirror
15 7, totally reflected by the lower face of the prism 10 and emerges from the face 13. It is then transmitted by the imaging lens 8 for visual line detection, thereby forming an image of the frontal part of the eye on the image sensor 9. The light reflected by the
20 cornea of the eye E forms Purkinje's images, while the light scattered by the pupil forms an image of the pupil. The visual line detecting circuit 14 calculates the direction of the visual line of the observer, based on the Purkinje's images and the pupil image obtained
25 from the image sensor 9. This detection can be achieved for example by a method disclosed in the Japanese Patent Laid-Open Application No. 3-109029 of

the present applicant.

The light source 12, the first optical member 3A, the prism 10, the imaging lens 8, the image sensor 9 and the visual line detecting circuit 13 constitute a part of the visual line detecting means.

Fig. 20 is a flow chart showing the control sequence of the present invention, for arbitrarily and selectively varying the size and position of the false image of the displayed image, to be superimposed with the external image, by the control means 16 of the present invention according to the visual line information of the eye E of the observer.

Fig. 21 is a schematic view of display areas, i.e. size and position of the display, selectable in the image display on the display means 4. In this embodiment there are selectable five display areas 1 to 5, in which 1 to 4 respectively correspond to rectangular areas, each equal to 1/4 of the display face, while 5 corresponds to the full display face.

In the following there will be explained the steps of the flow chart. The drawings at the right indicate the images provided to the observer at the respective steps.

In the present embodiment, the direction of the visual line of the observer is constantly detected.

Step 21: Turns on a switch for activating the function of the present invention. For this purpose,

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If the detected direction coincides with the switch mark, the discrimination means 15 judges that the observer has watched the switch mark for the predetermined time, and sends a signal to the control means 16 to turn on the switch. Then the sequence

proceeds to a step 22.

On the other hand, if the detected direction does not coincide with the switch mark, the sequence returns to (1).

5 By repeating the above-explained steps, the switching operation for the displayed image is securely started when the observer watches the switch mark for the predetermined time.

10 Step 22: When the switch is turned on, the control means 16 displays, for example, five points shown in Fig. 22, on the display face of the display means 4. Thus the observer sees an image 22a in Fig. 20.

15 Step 23: Determines the display area. The observer watches a point, representing the desired display area, for a predetermined time, and the visual line detecting means and the discrimination means 15 identifies the point watched by the observer for the predetermined time, within the image 22a, in the following sequence:

20 (1) The visual line detecting means detects the direction watched by the observer, and the discrimination means 15 identifies whether the detected direction coincides with any of the five points.

25 If the detected direction coincides with any of the points, the detected direction or position is stored, as first visual line information, in a memory.

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If the detected direction does not coincide with any of the points, the detection of the visual line is continued until the visual line is detected to any of the points.

5 (2) After the lapse of a predetermined time, the discrimination means 15 detects, by the visual line detecting means, the direction watched by the observer, and obtains second visual line information.

10 (3) The discrimination means 15 compares the detected direction of visual line with that corresponding to the point stored in the memory.

15 If two directions mutually coincide, the discrimination means judges that the point corresponding to the detected direction is the point desired by the observer for image display and sends the corresponding information to the control means 16, and the sequence proceeds to a step 24.

 If the two directions do not mutually coincide, the sequence returns to (1).

20 The point watched by the observer is determined by repeating the above-explained steps.

 In this manner, when the observer watches a point for a predetermined time, a display area is uniquely determined corresponding to said point.

25 Step 24: The control means 16 displays an image in the display area determined in the step 23, by varying the size and position of the display of the

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image, by applying suitable image processing to the image information. For example, if the point 5 shown in Fig. 21 is selected, the image is displayed in full size of the display face. If the point 4 is selected, the image size is changed to 1/4 of the display face and is displayed at the lower right part thereof, as shown in 24a. However the switch mark is separately displayed anew.

The switching of the displayed image is thus completed.

In the present embodiment, as explained in the foregoing, the size and position of the false image of the displayed image to be superimposed can be varied, in the course of image observation and according to the situation of the external image, by merely directing the visual line of the observer to a specified position within the viewing field, without any manual operation, so that there is attained extremely satisfactory operability. Besides, in the present embodiment, the entire device can be compactized by partial common use of the image observation optical system for observing the displayed image and the visual line detecting optical system for visual line detection.

In the foregoing embodiment the display area can be selected in five manners, but it is also possible to further increase the freedom of selection available to

the observer.

Also the switch turn-on operation may be conducted manually.

5 Figs. 23A and 23B are respectively schematic views showing optical paths in an observation optical system and a visual line detecting optical system in another optical system of the present invention, wherein components same as those in Figs. 19A and 19B are represented by same numbers.

10 The present embodiment is different from that shown in Figs. 19A and 19B in that a transmissive liquid crystal device (shield member) 11 is provided outside the face 6 of the second optical member in order to intercept the light beam, or a part thereof,
15 entering the prism block 3 from the outside. Such interception of the incoming light eliminates the overlapping of the external image with the false image Y of the displayed image, thereby enabling clear observation of the latter.

20 The prism 10, the first optical member 3A etc. constitute a part of the image observation optical system, while the image observation optical system, the second optical member 3B and the liquid crystal device 11 constitute a part of the observation optical system.
25 Also the light source 12, the first optical member 3A, the prism 10, the imaging lens 8, the image sensor 9 and the visual line detecting circuit 14 constitute a

The function of displayed image observation by the image observation optical system and that of the visual line detecting optical system in the present embodiment are same as that in the foregoing embodiment shown in Figs. 19A and 19B.

In the present embodiment, the direction of visual line of the observer is constantly detected.

Step 62: Enters the display size information of
25 the displayed image. The control means 16 displays,
for example, a false image of a displayed image 62a,
for observation by the observer. Said image includes,

for example, a full-sized rectangular display frame S1, a rectangular frame S2 which is 1/2 in size in the vertical and horizontal directions, and a rectangular frame S3 which is 1/4 in size.

5 Each display frame has a watching mark at a corner (upper right corner in the illustrated example). When the observer watches, for a predetermined time, the watching mark belonging to a desired frame, the visual line detecting means and the discrimination means 15
10 detect such watching state and judge that the observer has selected the corresponding display size, whereupon the display size is determined and the corresponding information is supplied to the control means 16.
15 (The sequence for this operation is similar to that already explained in the step 23 of the foregoing embodiment.) Such selecting procedure from a limited number of display frames enables rapid setting of the display size, though fine adjustment of the display size is not possible. As an example, let us consider
20 a case of selecting the frame S2.

Step 63: Enters the display position information of the displayed image. The control means 16 displays, for example, a false image of a displayed image 63a, in which the full-sized display face is divided into
25 grating-patterned areas of a suitable number, in superposition with the external image. Then the observer watches, for a predetermined time, a desired

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image display position (for example marked with "x")
in these areas. In response, the visual line detecting
means and the discrimination means 15 determine the
display position in the following sequence:

5 (1) The visual line detecting means detects the
position watched by the observer in the grating
pattern, and the discrimination means 15 stores the
detected area number, as first visual line information,
in a memory.

10 (2) After the lapse of a predetermined time, the
discrimination means 15 detects, by the visual line
detecting means, the position watched by the observer
in the grating pattern, and the detected area number
is taken as second visual line information.

15 (3) The discrimination means 15 compares thus
detected area number with that stored in the memory.

If the two area numbers mutually coincide, the
discrimination means 15 judges this area as the image
display area desired by the observer, and sends the
20 corresponding information to the control means 16.
Then the sequence proceeds to a step 64.

If the two area numbers do not coincide each
other, the memorized area number is replaced by the
newly detected area number, and the sequence returns
25 to (2).

The display position desired by the observer is
determined by repeating the above-explained steps.

This procedure enables secure entry of the position information and avoids erroneous input, even if the visual line of the observer is somewhat shifted, as long as the observer watches the vicinity of the
5 desired area for a predetermined time during the input state of the position information.

Step 64: The control means 16 discriminates whether the image of the designated size can be displayed around the display position designated by
10 the observer.

If such display is possible, the display area is thus determined and the sequence proceeds to a step 65.

On the other hand, if the displayed image P1 around the designated position overflow the display
15 face as indicated in 64a, the sequence proceeds to a step 66.

Step 66: Effects calculation for shifting the display position of the displayed image P1, for determining a display area P2, allowing to retain the
20 designated size of the image P1 with a minimum shift of the display position.

Step 65: The control means 16 shifts the transmittance of the liquid crystal device 11 to zero in the image overlapping portion as indicated in 65a,
25 thereby shielding the external image in said portion and avoiding the interference of the external image with the false image of thus determined display image.

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observer on the linear pattern. In this manner the observer can enter, in considerably precise manner, the proportion of display size with respect to the maximum display size.

5 In the present embodiment, a grating pattern is displayed at the entry of the display position, but such grating pattern display may be dispensed with.

 Based on the above-explained configuration, the present invention provides an observation optical
10 device of excellent operability capable of arbitrarily varying the size and position of display of the false image for observation of the image displayed on the display face, in the course of observation of such false image or of observation of such false image
15 spatially overlapped with the external image, to specified positions within the viewing field, according to the wish of the observer or to the external situation, utilizing the visual line of the observer.

20 Furthermore there is provided an observation optical device capable of shielding a part of the external image where the false image of the displayed image is overlapped, thereby enabling extremely clear observation of such false image.

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